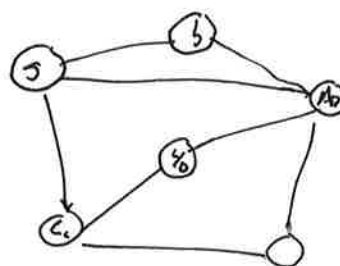
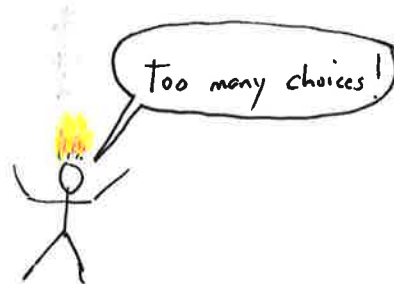


Primary Design Variables?

- Wing span $\equiv b$
- Wing Area $\equiv S$
- Aspect Ratio $\equiv AR$
- Flight Velocity $= V$
- Taper Ratio $= \lambda$
- Tail Length $= l_t$
- Tail Area $= S_h$
- Airfoil $\left\{ \begin{array}{l} \text{thickness} = \\ \text{Camber} = ? \\ \dots \end{array} \right.$
- Dihedral $= \Gamma$
- Wing Sweep $= \Lambda$
- Configuration $\equiv \left\{ \begin{array}{l} \text{monoplane} \\ \text{biplane} \\ \text{canard} \\ ? \end{array} \right.$
- Flight C_L
- Balsa $\left\{ \begin{array}{l} \text{Weight} = ? \\ \text{Thickness} = ? \end{array} \right.$

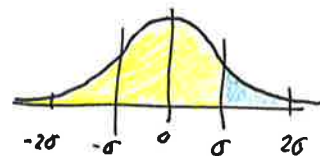


Pareto's Law

80% of results determined by 20% of actions

$$(.80^2 = 0.64 \quad \text{by} \quad .20^2 = 0.04)$$

Think of standard deviations



Simplify

$$AR \equiv \frac{b^2}{S}, \text{ so track } \left\{ \begin{array}{l} b, S \\ b, AR \\ S, AR \end{array} \right.$$

pick one

~~b, S, AR~~

$$W = L = \rho S C_L = \frac{1}{2} \rho V^2 S C_L$$

$$Re \approx 6350 \cdot V \cdot \bar{c} \quad \text{unless } \lambda \neq 1$$

Endurance



From AEM 368, the vertical velocity is

$$\dot{h} = V_\infty \left(\underbrace{\frac{T}{W}}_{\text{thrust}} - \underbrace{\frac{1}{2} \rho V_\infty^2 \left(\frac{W}{S}\right)^{-1} C_{D_0}}_{\text{profile drag}} - \underbrace{\frac{W}{S} \frac{2k \cos^2 \theta}{\rho V_\infty^2}}_{\text{induced drag}} \right)$$

Simplify for a glider ($T=0$, $\cos^2 \theta \approx 1$)

$$\dot{h} = V_\infty \left(-\frac{1}{2} \rho V_\infty^2 \left(\frac{W}{S}\right)^{-1} C_{D_0} - \frac{W}{S} \frac{2k}{\rho V_\infty^2} \right)$$

Optimize \dot{h} wrt V_∞ (calculus ... set derivative to zero)

$$\frac{d\dot{h}}{dV_\infty} = -\frac{1}{2} 3 \rho V_\infty^2 \left(\frac{W}{S}\right)^{-1} C_{D_0} + \left(\frac{W}{S}\right) \frac{2k}{\rho V_\infty^3} = 0$$

$$V_{\infty \dot{h}_{\min}} = \sqrt{\frac{2}{\rho} \sqrt{\frac{k}{3C_{D_0}} \frac{W}{S}}}$$

$$V_v = \sqrt{\frac{2}{\rho} \frac{1}{C_L^3/C_D^2} \frac{W}{S}} = \frac{C_D}{C_L^{3/2}} \sqrt{\frac{2}{\rho} \frac{W}{S}} = V_v$$

For maximum endurance, you want:

- Large $C_L^{3/2}/C_D$
- Low W/S

$\left(\frac{C_L}{C_D}\right)_{\max}$ occurs at

$$V_\infty = \sqrt{\frac{2}{\rho} \frac{W}{S} \sqrt{\frac{k}{3C_{D_0}}}}$$

with value

$$\left(\frac{C_L}{C_D}\right)_{\max} = \frac{1}{4} \left(\frac{3}{k C_{D_0}^{3/2}}\right)^{3/4}$$

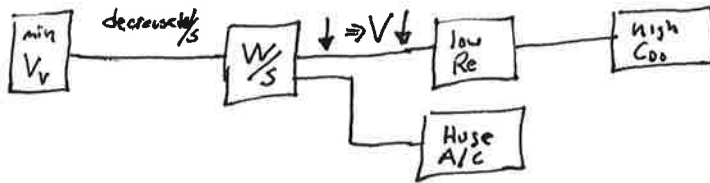
$$V_{V_{min}} = 4 \left(\frac{k C_{D_0}^{3/2}}{3} \right)^{3/4} \sqrt{\frac{2}{\rho} \frac{W}{S}} \quad \text{at } V_{\infty} = \sqrt{\frac{2}{\rho} \frac{W}{S}} \sqrt{\frac{k}{3 C_{D_0}}}$$

with this model of the aerodynamics, you want

- Low drag C_{D_0} .
- Low wing loading W/S

Problems / Trade-Offs

Wing area:



Drag

Notice that $(C_{D_0}^{3/2})^{3/4} \approx C_{D_0}^{9/8} \approx C_{D_0}$

Structure

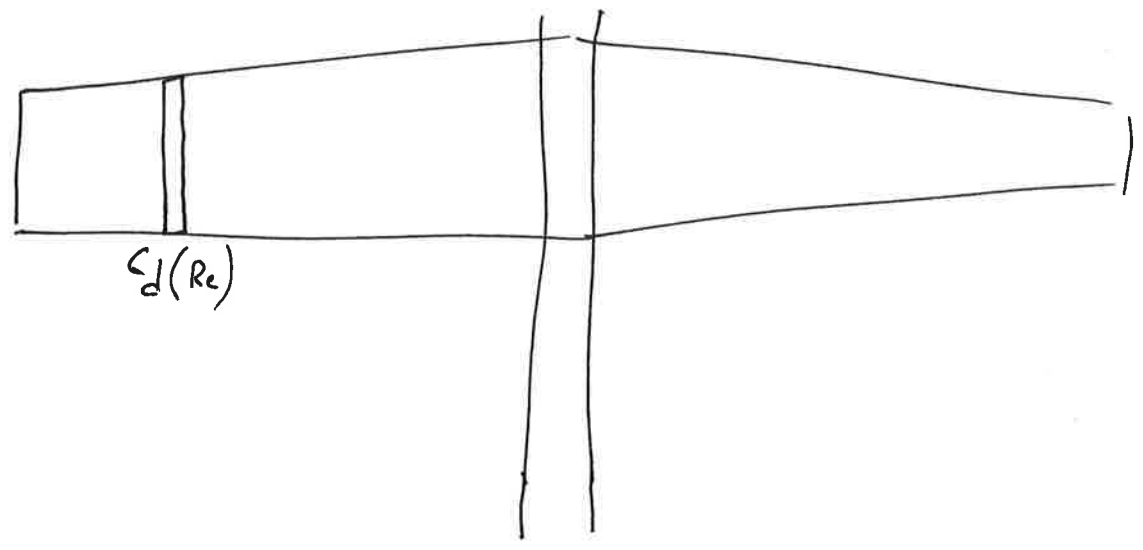
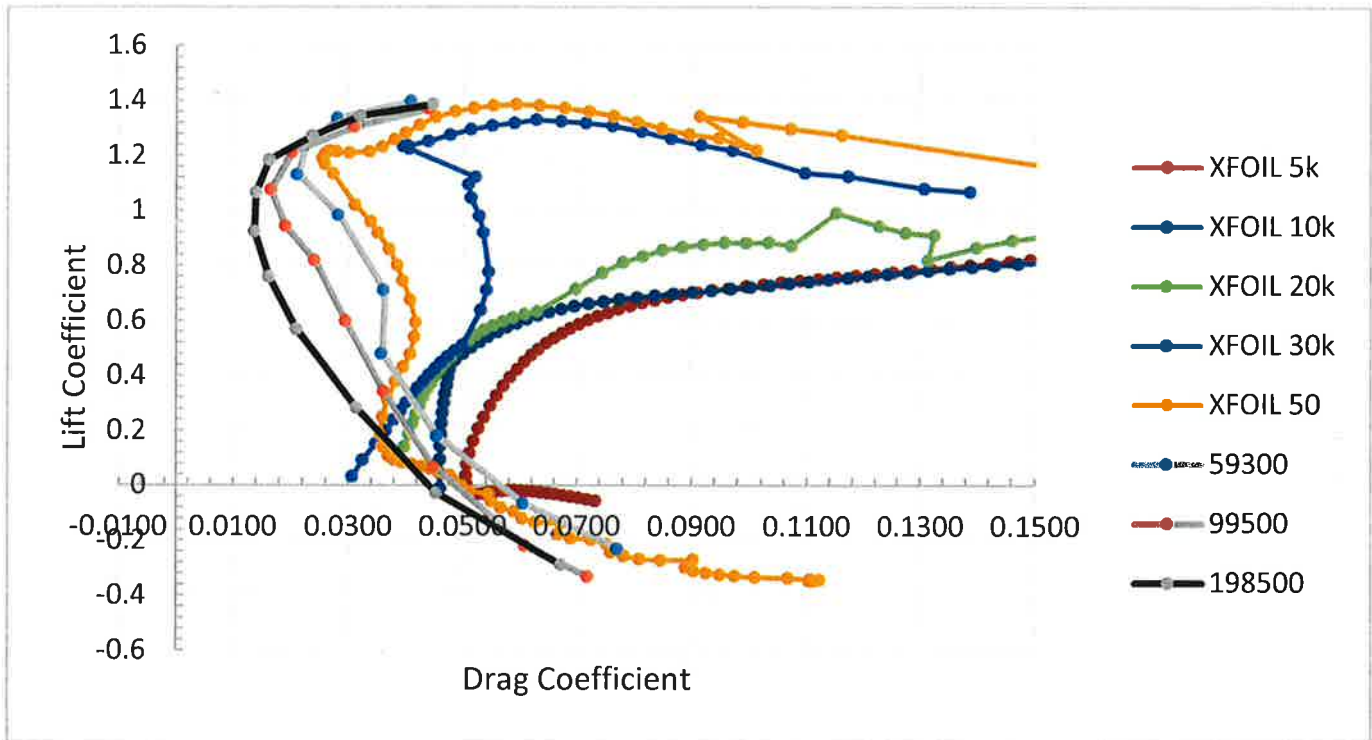
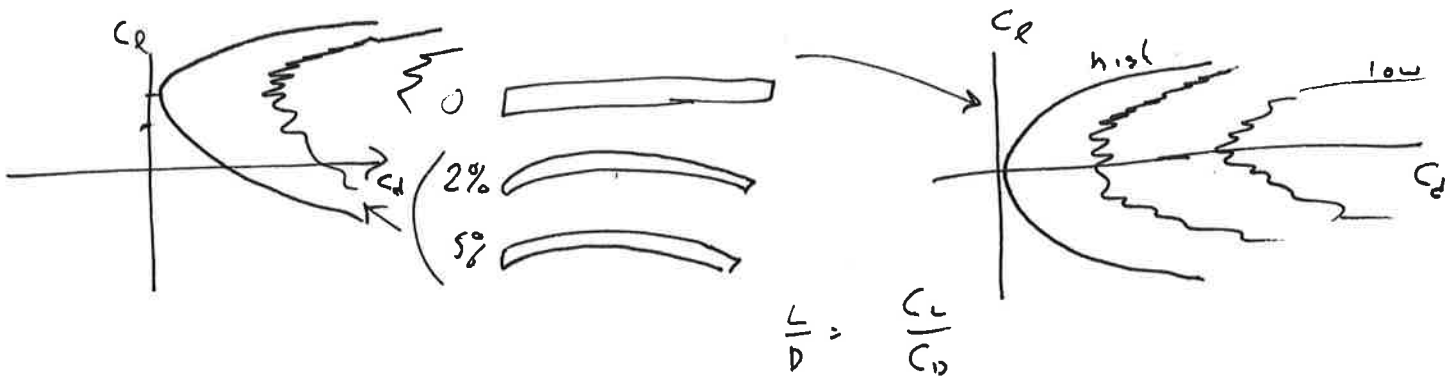
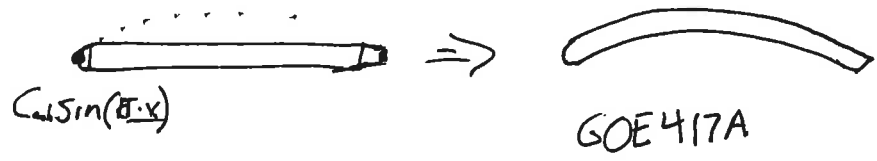
- paper and foam are low-performance materials (low E , low ultimate)

A large ~~big~~ wing area will give a big floppy twisting aircraft. (i.e. high C_{D_0} , untrimmed)

- Difficult to form smooth airfoils. (or even cambered airfoils)
- Highest density objects are the 25¢ quarters. These can provide an advantage for weight + balance.

Remember, you must have the Center of Gravity ahead of the aircraft's Neutral Point / Aerodynamic Center. Make the horizontal tail large enough!

The most common failures will be unstable aircraft and wings folding
 needs C.G and tail area fixed keep smaller S and test prior to competition



Excel spreadsheet

primary design variables

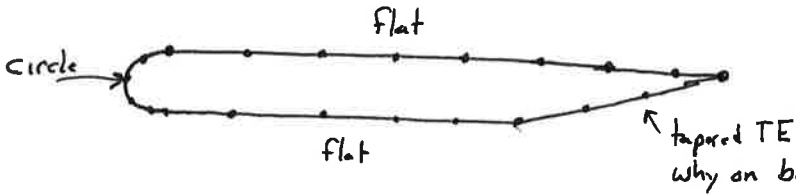
C_L , b , AR , airfoil

everything else is calculated from these.

C_L	b	AR	S	$\lambda=1$ \bar{c}	C_{Di}	V	Re	$C_{D_{0_{wing}}}$	C_D	L/D	$L/D^{3/2}$
			$= \frac{b^2}{AR}$	$= \frac{S}{b}$	$= \frac{C_L^2}{\pi AR c}$	$\sqrt{\frac{2W AR}{\rho C_L b^2}}$	$6350 V \bar{c}$	lookup from XFOIL at Re and C_L	$C_{Di} + C_{D_0}$	$\frac{C_L}{C_D}$	$\frac{C_L^{3/2}}{C_D}$

$$\frac{L^{3/2}}{D} \sqrt{\frac{W}{S}}$$

Airfoils?



why on bottom? BL sensitivity is less to $\frac{d\theta}{d\alpha}$ when θ is smaller! θ is smaller why? less acceleration....

Transform via camber line

Camber $\left\{ \begin{array}{l} \text{sin}(\pi x) \cdot \text{Camber} = Z^+ \Rightarrow Z_{\text{new}} = Z_{\text{flat}} + Z^+ \end{array} \right.$

you can pick the camber function....