

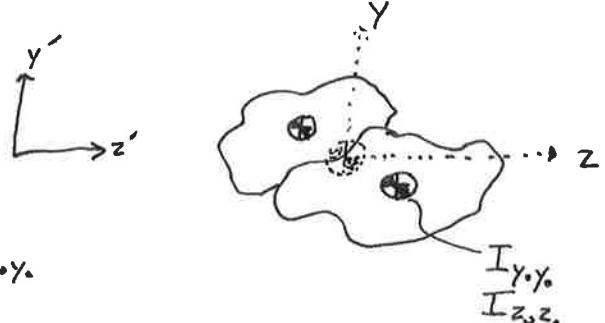
How to find the centroid and I_{yy} I_{zz} moments of inertia of an advanced beam.

① Centroid

- Decompose into parts
- With respect to any coordinate system origin
- $\sum A_i$ sum areas of each part
- $\sum z_i A_i$ sum (distance from centroid of each part) · (area of each part)
- Centroid is at $\frac{\sum z_i A_i}{\sum A_i}$

② Moments of inertia

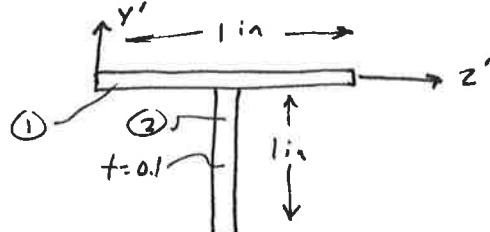
- With respect to $y'z'$
- Determine $\sum y_i'^2 A_i$ and $\sum I_{y,y}$
- $I_{y'y} = \sum I_{y,y} + \sum z_i'^2 A_i$
- $I_{yy} = I_{y'y} - z'^2 A$ Shift to centroid



Notice that this is much easier than shifting each part to the centroid (even if the result is eventually identical)

See example 4.1 (critical to understand)

Ex: T beam



$$I_{0yy} = \frac{1}{12} b h^3 = \frac{1}{12} 0.1 \cdot 1^3 = 0.00833$$

$$I_{0zz} = \frac{1}{12} l \cdot 0.1^3 = 8.3 \times 10^{-5}$$

① Centroid

Part	Area	z'	y'	$z'A$	$y'A$
1	0.1	0.5	0	0.05	0
2	0.1	0.5	-0.5	0.05	-0.05
$\underline{\underline{0.2}}$				$\underline{\underline{0.1}}$	$\underline{\underline{-0.05}}$

$$\bar{z}' = \frac{0.1}{0.2} = 0.5$$

$$\bar{y}' = \frac{-0.05}{0.2} = -0.25$$

② MoI

$\brace{ \text{of part} }_{\text{distance to centroid from } y'}$

Part	A	\bar{y}'	\bar{z}'	$\bar{y}'^2 A_i$	$\bar{z}'^2 A_i$	I_{yy_0}	I_{zz_0}
1	0.1	0	0.5	0	0.025	0.00833	8.3 \times 10^{-5}
2	0.1	-0.25	0.5	0.00625	0.025	8.3 \times 10^{-5}	0.00833
$\underline{\underline{0.00625}}$				$\underline{\underline{0.05}}$	$\underline{\underline{0.00842}}$	$\underline{\underline{0.00842}}$	

$$I_{yy'} = \sum I_{yy_0} + \sum y_i^2 A_i = 0.00842 + 0.05 = 0.05842$$

$$I_{zz'} = \sum I_{zz_0} + \sum z_i^2 A_i = 0.00842 + 0.00625 = 0.01467$$

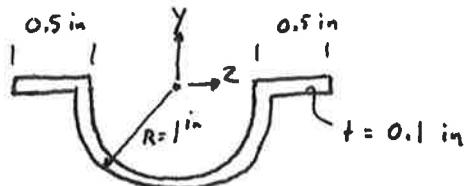
$$I_{y'z'} = \sum I_{y_0 z_0} + \sum y_i z_i A_i = 0$$

Shift to centroid of beam

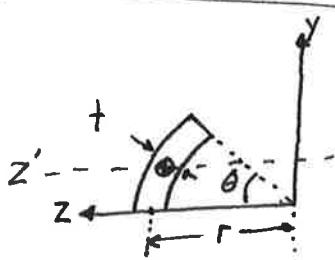
$$I_{yy} = I_{yy'} - \bar{z}'^2 A = 0.05842 - 0.5^2 \cdot 0.2 = 0.00842$$

$$I_{zz} = I_{zz'} - \bar{y}'^2 A = 0.01467 - 0.25^2 \cdot 0.2 = 0.00217$$

Ex: U channel



Write in your book (p 500)



$$A = rt\theta$$

$$z' = \frac{r}{\theta} (1 - \cos \theta)$$

$$I_{zz} = r^3 t \left(\frac{\theta - \sin \theta \cos \theta}{2} \right)$$

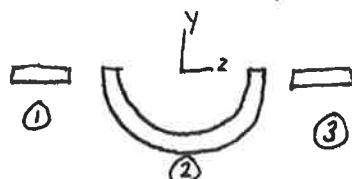
$$I_{z'z'} = r^3 t \left(\frac{\theta - \sin \theta \cos \theta}{2} \right) - \frac{r^3 t}{\theta} (1 - \cos \theta)^2$$

θ is in radians

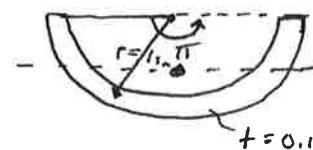
r is median line (i.e. half thickness)

- Find \bar{y} , \bar{z} , and I_{yy} , I_{zz} , I_{yz}

① Centroid



part ②



part	Area	z'	$z' \cdot \text{Area}$
1	0.04	0	0
2	0.314159	-0.63662	-0.2
3	0.04	0	0
\sum		0.3942	$\sum -0.2$

$$z' = \frac{1 \cdot \pi}{3.1415} (1 - \cos \pi)$$

$$= \frac{2}{\pi} = 0.63662$$

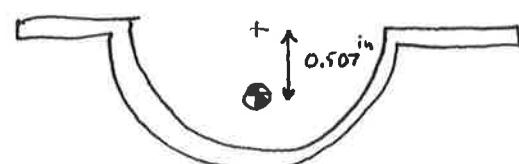
$$A = \frac{1}{3.1415} \cdot 0.1 = 0.3141$$

$$\bar{y}' = \frac{\sum z' A}{\sum A} = \frac{-0.2}{0.3942} = -0.507$$

- \bar{z} By inspection = 0

Part	Area	z'	$z' A$
1	0.04	0	0
2	0.31415	0	0
3	0.04	0	0
\sum		0.3942	$\sum 0$

$$\bar{z} = \frac{0}{0.3942} = 0$$



② MoI

Part	Area	y'	z'	$y'^2 A$	$z'^2 A$	I_{y,y_0}	I_{z,z_0}
1	0.04	0	1.2	0	0.0576	0.000533	≈ 0
2	0.314	-0.636	0	0.127	0	0.15708	0.15708
3	0.04	0	-1.2	0	0.0576	0.000533	≈ 0
					<u>0.1152</u>		

$$I_{yy'} = 0.158 + 0.1152 = 0.2723$$

$$I_{zz'} = 0.15708 + 0.127 = 0.284$$

Shift to beam centroid

$$I_{yy} = 0.2723 - 0^2 \cdot 0.3942 = 0.2723$$

$$I_{zz} = 0.284 - 0.507^2 \cdot 0.3942 = 0.1827$$

Rotational Transform of M. I

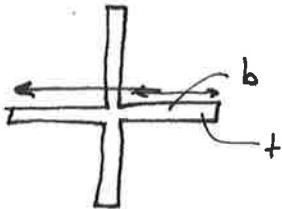
$$I_{xx}^* = \frac{I_{xx} + I_{yy}}{2} + \frac{I_{xx} - I_{yy}}{2} \cos 2\theta - I_{xy} \sin 2\theta$$

$$I_{yy}^* = \frac{I_{xx} + I_{yy}}{2} - \frac{I_{xx} - I_{yy}}{2} \cos 2\theta + I_{xy} \sin 2\theta$$

$$I_{xy}^* = \frac{I_{xx} - I_{yy}}{2} \sin 2\theta + I_{xy} \cos 2\theta$$

where have you
seen this before?!

Ex:



Identical legs.

Is there a "weak" direction of bending?

① By symmetry $I_{yy} = I_{zz} \approx \frac{1}{12} + b^3$

② Rotate by θ

$$I_{yy}^* = \frac{\cancel{I_{yy}} + \cancel{I_{zz}}}{2} + \frac{\cancel{I_{yy}} - \cancel{I_{zz}}}{2} \cos 2\theta - \cancel{I_{yy}} \sin 2\theta = \frac{1}{12} + b^3 = I_{yy}$$

same for I_{zz}^* and $I_{xy}^* = 0$

Same bending stiffness regardless of rotation

Ex: Beam

$$I_{yy} = \frac{1}{12} b h^3 \Rightarrow \frac{I_{zz}}{I_{yy}} = \frac{\frac{1}{12} b h^3}{\frac{1}{12} b h^3} = \frac{h^2}{b^2}$$

$$= \left(\frac{h}{b}\right)^2$$

What is the M.o.I wrt twist? Assume $\frac{h}{b} \gg 1 \approx 10$

$$I_{yy'} = \underbrace{\frac{I_{yy} + I_{zz}}{2}}_{\frac{I_{zz}}{2}} + \underbrace{\frac{I_{yy} - I_{zz}}{2} \cos 2\theta}_{-\frac{I_{zz}}{2} \cos 2\theta} - \underbrace{I_{xy} \sin 2\theta}_0$$

$$= \frac{I_{zz}}{2} (1 - \cos 2\theta)$$

$$I_{zz'} = \frac{I_{yy} + I_{zz}}{2} - \frac{I_{yy} - I_{zz}}{2} \cos 2\theta + \underbrace{I_{yz} \sin 2\theta}_0$$

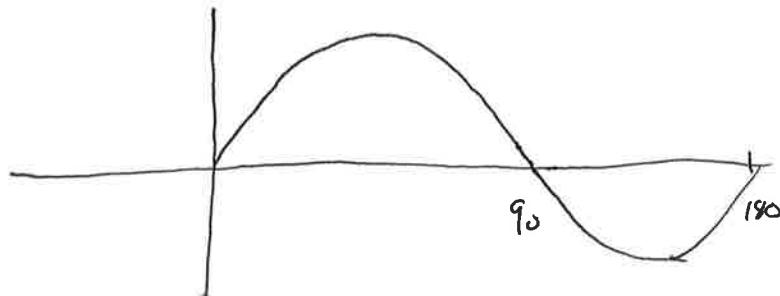
$$\approx \frac{I_{zz}}{2} + \frac{I_{zz}}{2} \cos 2\theta =$$

$$= \frac{I_{zz}}{2} (1 + \cos 2\theta)$$

$$I_{yz'} = \frac{I_{yy} - I_{zz}}{2} \sin 2\theta + \underbrace{I_{yz} \cos 2\theta}_0$$

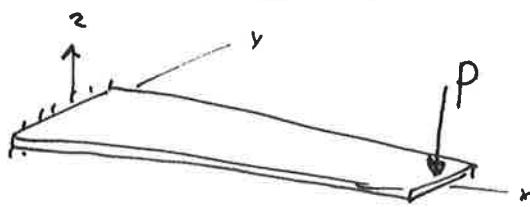
$$\approx -\frac{I_{zz}}{2} \sin 2\theta$$

$\frac{h}{b} > 1$
If a beam twists during loading,
the M.o.I can decrease



Twist Bend Buckling of beams

from Advanced Strength of Materials
Don Hartog



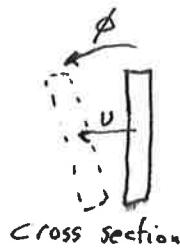
Low I_{yy}
More bending



High I_{yy}
less bending

Compare
What if the loading causes the beam to twist?

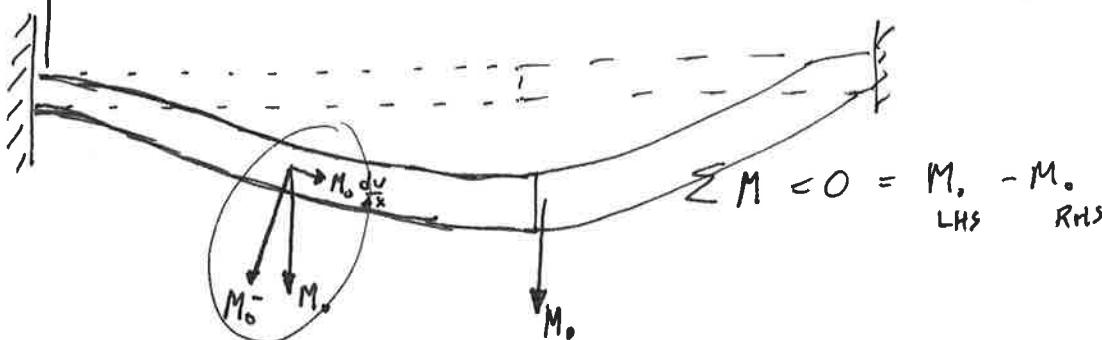
Stable?



I_{yy} is lower and there is a new moment generated!

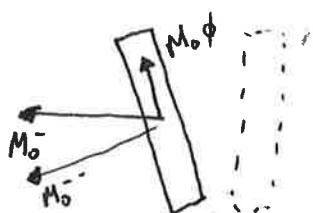
Pinned-Pinned Beam

Top view M_0



But we can decompose the moment to moments along the beam's frame (since there is twisting and deflection)
sideways

End View



Decompose M_0 into beam frame

Solving the bending and twisting equations

$$EI\psi'' = -M_o \phi \quad + \underbrace{\frac{Ght^3}{3}\phi}_{C} = M_o u'$$

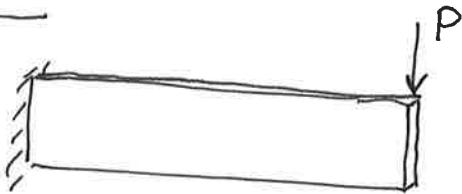
gives a solution

$$\phi = \text{Constant} \cdot \sin \left(x \frac{M_o}{\sqrt{EI \cdot C}} \right)$$

The critical case is when this is π

$$M_{\text{crit}} = \frac{\pi \sqrt{EI \cdot C}}{l}$$

Cantilever Beam



The math is much more complicated

Buckles at

$$P_{\text{crit}} = \frac{4.01}{l^2} \sqrt{G \frac{1}{3} h t^3 E \frac{h t^3}{12}} \approx \frac{0.67 h t^3}{l^2} \frac{E}{\sqrt{2(1+\nu)}}$$

Failure?

Buckle or Yield?

$$P_{\text{crit}} \quad \sigma = \frac{My}{I}$$

Ex:

What is the buckling load for a 3 foot spar of height 1" and thickness 0.1 in. The spar is Al.

$$P_{\text{crit}} = \frac{0.67}{36^2 \text{ in}^2} \left| \frac{1 \text{ in}}{0.1^3 \text{ in}^3} \right| \left| \frac{10 \times 10^6 \text{ psi}}{\sqrt{2(1+0.3)}} \right| \frac{16 \text{ ft}}{\text{psf in}^2}$$

$$= 3^{16} \text{ ft}$$

Ex. What is the max stress? $M = 36 \cdot F \quad I = \frac{1}{12} \cdot 0.1 \cdot 1^3 = 0.00833$

$$\sigma = \frac{My}{I} = \frac{36 \cdot F \cdot 0.5}{0.00833} = 6.4 \text{ ksi}$$

Buckles