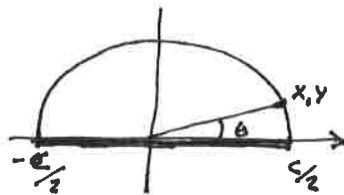


Lesson 10 part 2

Thin Airfoil Theory

# Thin Airfoil Theory - Part 2

Cosine spacing - a coordinate transform from  $x$  to  $\theta$

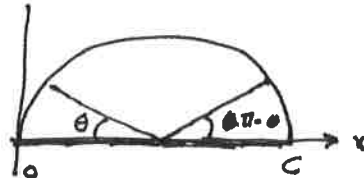


$$X = \frac{c}{2} \cos \theta \Rightarrow dx = -\frac{c}{2} \sin \theta d\theta$$

$$X_{LE} \text{ at } \theta = \pi$$

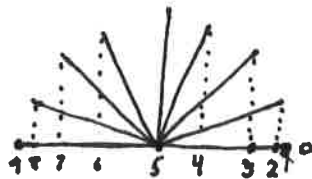
$$X_{TE} \text{ at } \theta = 0$$

or



$$X = \frac{c}{2} (1 - \cos \theta) \Rightarrow dx = \frac{c}{2} \sin \theta d\theta$$

This transform is common in aerodynamics. This is also an excellent way to place points on a line segment when you need more resolution at the ends.



$$8 \text{ steps} \Rightarrow \Delta\theta = \frac{\pi}{8} = 22.5^\circ$$

9 points at

~~0%, 12.5%, 25%, 37.5%, 50%, 62.5%, 75%, 87.5%, 100%~~  
0%, 3.8%, 15%, 30%, 50%, 70%, 85%, 97%, 100%

There are even an entire class of polynomials that exploit this transform called the Chebyshev polynomials

$$T_n(\cos \theta) = \cos(n\theta)$$

These are orthogonal and satisfy the following ODE

$$(1-x^2)y'' - xy' + n^2y = 0$$

In fact, it has been suggested that if you are not working with harmonic data, the Chebyshev polynomial is ideal (cf. Boyd, Spectral Methods...)

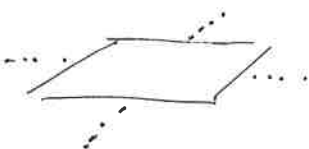
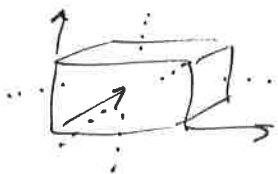
They also have a recurrence equation

$$T_0(x) = 1, T_1(x) = x, T_{n+1}(x) = 2xT_n(x) - T_{n-1}(x)$$

# Source and Vortex Sheets in 2D and their perturbation velocities

$$\sigma = \nabla \cdot \mathbf{V} \quad \text{reverse} \Rightarrow$$

$$\omega = \nabla \times \mathbf{V}$$



$$V_{\sigma}(\mathbf{r}) = \frac{1}{4\pi} \iiint \sigma(\mathbf{r}') \frac{\mathbf{r} - \mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|^3} dx' dy' dz'$$

$$V_{\omega}(\mathbf{r}) = \frac{1}{4\pi} \iiint \omega(\mathbf{r}') \times \frac{\mathbf{r} - \mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|^3} dx' dy' dz'$$

↓ sheets

$$V_{\sigma}(\mathbf{r}) = \frac{1}{4\pi} \iint \lambda \frac{\mathbf{r} - \mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|^3} ds dz'$$

↓ 2D sheets

$$V_{\sigma}(\mathbf{r}) = \frac{1}{2\pi} \iint \sigma(\mathbf{r}') \frac{\mathbf{r} - \mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|^2} dx' dz'$$

$$V_{\omega}(\mathbf{r}) = \frac{1}{2\pi} \iint \omega(\mathbf{r}') \frac{\hat{\mathbf{y}} \times (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^2} dx' dz'$$

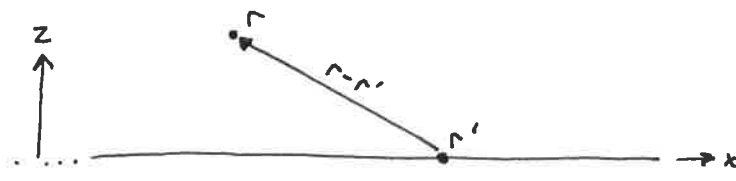
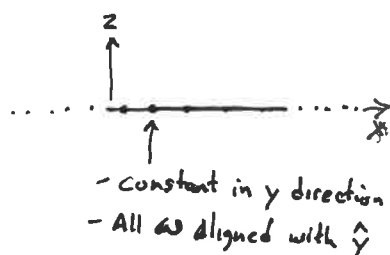
Notice

$$|\mathbf{r} - \mathbf{r}'|^2$$

not

$$|\mathbf{r} - \mathbf{r}'|^3$$

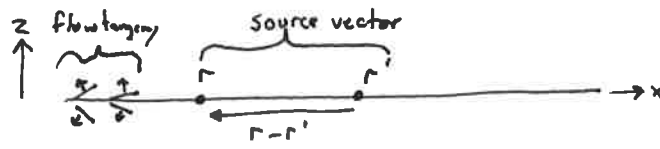
and  
 $\frac{1}{2\pi}$  vs  $\frac{1}{4\pi}$



$$\mathbf{r} - \mathbf{r}' = (x - x')\hat{\mathbf{x}} + (z - z')\hat{\mathbf{z}}$$

$$|\mathbf{r} - \mathbf{r}'| = \sqrt{(x - x')^2 + (z - z')^2}$$

Now we see the visual definition of "thin airfoils". All source and vortex properties are determined at and along the x axis, (i.e.  $z - z' = 0$ ). Even flow tangency is applied at  $z = 0$



$$\mathbf{r} - \mathbf{r}' = (x - x')\hat{\mathbf{x}}$$

$$|\mathbf{r} - \mathbf{r}'| = \sqrt{(x - x')^2} = |x - x'|$$

$$V_{\sigma}(x) = \frac{1}{2\pi} \int \sigma(x') \frac{(x - x')\hat{\mathbf{x}}}{(x - x')^2} dx' = \frac{1}{2\pi} \int \sigma(x') \frac{dx'}{x - x'} \hat{\mathbf{x}}$$

$$V_{\omega}(x) = \frac{1}{2\pi} \int \omega(x') \frac{\overbrace{\hat{\mathbf{y}} \times (x - x')\hat{\mathbf{x}}}^{\hat{\mathbf{y}} \times \hat{\mathbf{x}} = -\hat{\mathbf{z}}}}{(x - x')^2} dx' = \frac{1}{2\pi} \int \omega(x') \frac{-dx'}{x - x'} \hat{\mathbf{z}}$$

# Perturbation Velocities

Source

$$V_\sigma = \frac{1}{2\pi} \int \sigma(x') \frac{dx'}{x-x'} \hat{x} \Rightarrow$$

$$U(x) = \frac{1}{2\pi} \int \sigma(x') \frac{dx'}{x-x'}$$

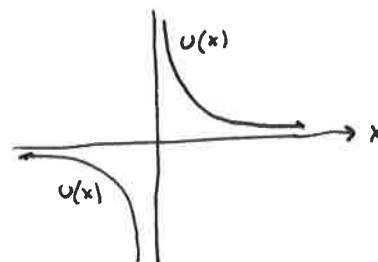
So, along the x axis (and not considering the jump), a source creates a perturbation in the U velocity. Important!

Example:

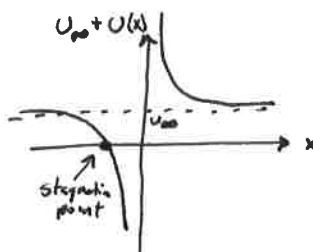
To illustrate this, pick a point source ( $\sigma(x') = \delta(x')$ ) =   $\int \delta = 1$

$$U(x) = \frac{1}{2\pi} \int \delta(x') \frac{dx'}{x-x'} \text{ only has value when } x' = 0$$

$$= \frac{1}{2\pi} \int \delta dx' \left( \frac{1}{x} \right) = \frac{1}{2\pi x}$$



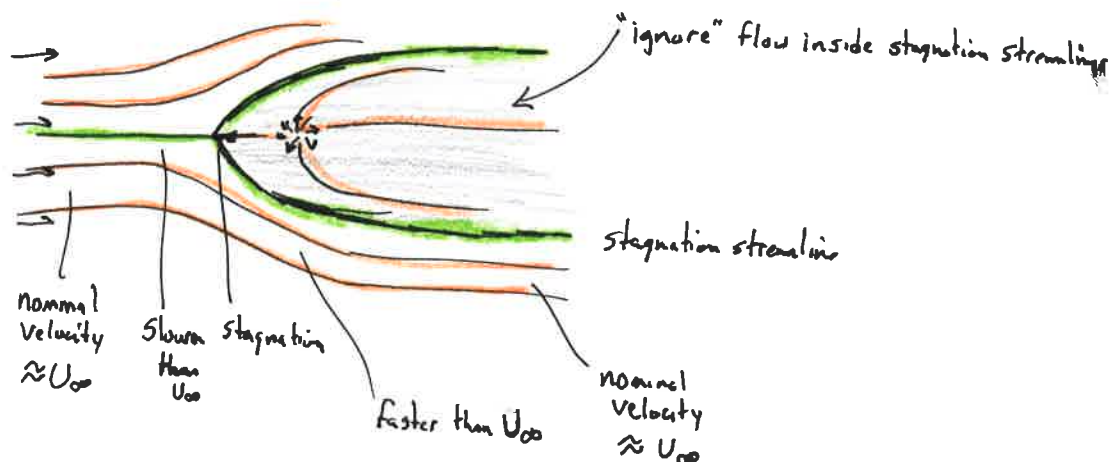
Add a free stream  $U_\infty$



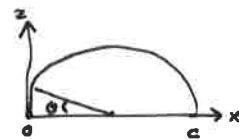
As we approach the point source, the flow velocity decreases to a stagnation point. Aft of the source, the flow velocity decreases from a higher velocity back to freestream.

We have here a proto-symmetrical airfoil.

If we plot in 2D, the streamfunction  $\Psi$  gives



Back to our thin airfoil with a cosine transform



$$x = \frac{c}{2}(1 - \cos \theta)$$

$$dx = +\frac{c}{2} \sin \theta d\theta$$

$$U(\theta) = \frac{1}{2\pi} \int_0^c \gamma(x') \frac{dx'}{x-x'} = \frac{1}{2\pi} \int_0^\pi \gamma(\theta') \frac{\frac{c}{2} \sin \theta d\theta}{\frac{c}{2}(1 - \cos \theta) - \frac{c}{2}(1 - \cos \theta')}$$

$$= \frac{1}{2\pi} \int_0^\pi \gamma(\theta') \frac{\sin \theta' d\theta'}{\cos \theta' - \cos \theta}$$

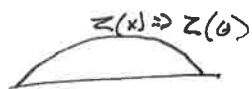
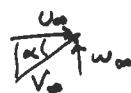
$$W(\theta) = \frac{1}{2\pi} \int_0^c -\gamma(x') \frac{dx'}{x-x'} = \frac{1}{2\pi} \int_0^\pi -\gamma(\theta') \frac{\sin \theta' d\theta'}{\cos \theta' - \cos \theta}$$

Substitute into

$$\frac{d}{dx}(U_\infty Z) = W_\infty + W$$

with  $W_\infty = V_\infty \sin(\alpha)$

$$U_\infty = V_\infty \cos(\alpha)$$



$$\frac{d}{dx}(V_\infty \cos \alpha Z) = V_\infty \sin \alpha + \frac{1}{2\pi} \int_0^\pi -\gamma(\theta') \frac{\sin \theta' d\theta'}{\cos \theta' - \cos \theta}$$

$$\boxed{\frac{dZ}{dx} = \alpha + \frac{1}{2\pi} \int_0^\pi -\frac{\gamma(\theta')}{V_\infty} \frac{\sin \theta' d\theta'}{\cos \theta' - \cos \theta}}$$

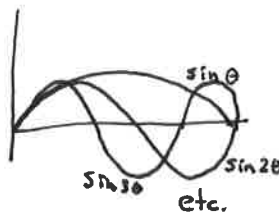
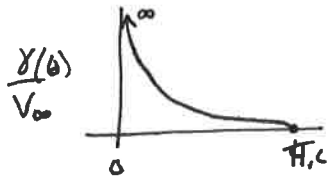
Apply Kutta condition

$$\gamma \Big|_\pi = 0$$

What is  $\gamma(\theta)$ ?

$$\frac{1}{2\pi} \int_0^\pi \frac{\gamma(\theta')}{V_\infty} \frac{\sin \theta' d\theta'}{\cos \theta' - \cos \theta} = A_0 - \sum_{n=1}^{\infty} A_n \cos n\theta$$

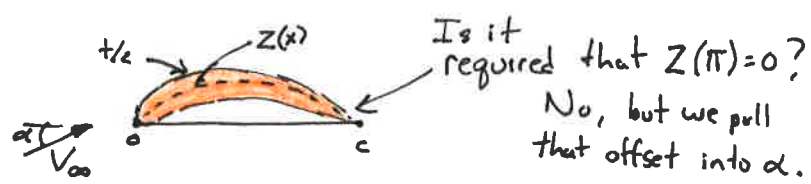
$$\frac{\gamma(\theta)}{V_\infty} = \underbrace{2 A_0 \frac{1 + \cos \theta}{\sin \theta}}_{\text{Graph 1}} + \underbrace{2 \sum_{n=1}^{\infty} A_n \sin n\theta}_{\text{Graph 2}}$$



What is  $\lambda(x)$ ?

$$\lambda(x) = V_\infty \frac{dt}{dx}$$

Thin airfoil



$$U_{\infty} \frac{dt}{dx} = \lambda$$

and

$$\frac{1}{2\pi} \int_0^{\pi} \frac{\gamma(\theta')}{V_{\infty}} \frac{\sin \theta' d\theta'}{\cos \theta' - \cos \theta} = \alpha - \frac{dZ(\theta)}{dx} \quad \text{with} \quad \gamma(\pi) = 0$$

Solution:

Represent  $\alpha - \frac{dZ(\theta)}{dx}$  with a Fourier series of cos.

$$\alpha - \frac{dZ(\theta)}{dx} = A_0 - \sum_{n=1}^{\infty} A_n \cos n\theta$$

Why cos? Well, we want  $Z(0) = Z(\pi) = 0$ , so a sine series in  $Z$  is a cosine series in  $\frac{dZ}{dx}$ .

From Fourier theory

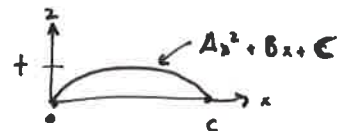
$$A_0 = \alpha - \frac{1}{\pi} \int_0^{\pi} \frac{dZ}{dx} d\theta \quad \text{and} \quad A_n = \frac{2}{\pi} \int_0^{\pi} \frac{dZ}{dx} \cos n\theta d\theta$$

If you can write  $\frac{dZ}{dx}$  as a Fourier series,  $Z$  is also a Fourier series.

Remember that

$$\int_0^{\pi} \cos n\theta \cos m\theta d\theta = \begin{cases} \pi & n=m=0 \\ \pi/2 & n=m \neq 0 \\ 0 & n \neq m \end{cases}$$

Ex:  $Z(x) = 4\frac{x}{c} - 4\frac{x^2}{c^2}$  for a parabolic camberline.



$$\frac{dZ(x)}{dx} = 4\frac{x}{c} - 8\frac{x}{c^2}$$

convert to cosine transform/space  $x = \frac{c}{2}(1 - \cos \theta)$

$$\frac{dZ(\theta)}{dx} = 4\frac{x}{c} - 8\frac{x}{c^2} = 4\frac{x}{c} \cos \theta = 4\frac{x}{c} \cos \theta$$

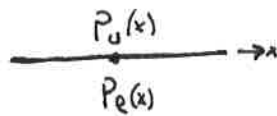


Match terms

$$A_0 = \alpha - \frac{1}{\pi} \int_0^{\pi} \dots d\theta \quad A_n = \frac{2}{\pi} \int_0^{\pi} 4\frac{x}{c} \cos \theta \cos n\theta d\theta$$

$$A_0 = \alpha, A_1 = 4\frac{x}{c}, A_2 = 0, A_3 = 0, \dots$$

# Forces and Moments



$$\Delta C_p = \frac{P_l - P_u}{\rho} \quad \text{from incompressible B'} \quad \Delta C_p = \frac{|V_u|^2 - |V_l|^2}{V_\infty^2}$$

From the velocity jump from the vortex sheet,

$$\Delta C_p \approx 2 \frac{\gamma}{V_\infty}$$

Lift:

$$C_L = \int_0^c \Delta C_p dx \approx \int_0^c 2 \frac{\gamma}{V_\infty} dx = \int_0^\pi \underbrace{\frac{\gamma}{V_\infty} \sin \theta d\theta}_{\text{cosine transform.}}$$

$$= \int_0^\pi 2 \left( A_0 \frac{1 + \cos \theta}{\sin \theta} + \sum_{n=1}^{\infty} A_n \sin n\theta \right) \sin \theta d\theta$$

with  $\int_0^\pi \sin \theta \cos \theta d\theta$  and  $\int_0^\pi \sin n\theta \sin m\theta d\theta \neq 0$  only when  $n=m$   
 $= \pi/2$  when  $n=m$

$$C_L = 2\pi A_0 + \cancel{\pi A_1} \pi A_1$$

$$= 2\pi \alpha + 2 \int_0^\pi \frac{dz}{dx} (\cos \theta - 1) d\theta$$

$$= 2\pi \alpha + C_{L_0} \quad \text{where } C_{L_0} \text{ depends on the camberline}$$



$$\boxed{\frac{dC_L}{d\alpha} = 2\pi}$$